

## 2.10 Criticality

The discussion of the criticality of a nuclear reactor will now be resumed. It is self-evident that a finite reactor will manifest an accelerating chain reaction when  $k > 1$  (or  $\rho > 0$ ); such a reactor is termed *supercritical*. Moreover a reactor for which  $k = 1$  ( $\rho = 0$ ) is termed *critical* and one for which  $k < 1$  ( $\rho < 0$ ) is *subcritical*. Note that since the neutron escape from a finite reactor of typical linear dimension,  $l$ , is proportional to the surface area,  $l^2$ , while the neutron population and production rate will be proportional to the volume or  $l^3$  it follows that  $k$  will increase linearly with the size,  $l$ , of the reactor and hence there is some *critical size* at which the reactor will become critical. It is clear that a power plant needs to maintain  $k = 1$  to produce a relatively stable output of energy while gradually consuming its nuclear fuel.

Consequently there are two sets of data that determine the criticality of a reactor. First there is the basic neutronic data (the fission, scattering and absorption cross-sections, and other details that are described previously in this chapter); these data are functions of the state of the fuel and other constituents of the reactor core but are independent of the core size. These so-called *material properties* of a reactor allow evaluation of  $k_\infty$ . The second set of data is the geometry of the reactor that determines the fractional leakage of neutrons out of the reactor. This is referred to as the *geometric property* of a reactor and this helps define the difference between  $k$  and  $k_\infty$ . These two sets of data are embodied in two parameters called the *material buckling*,  $B_m^2$ , and the *geometric buckling*,  $B_g^2$ , that are used in evaluating the criticality of a reactor. These will be explicitly introduced and discussed in chapter 3.